

Bio4Fuels

Norwegian Centre for Sustainable Bio-Based Fuel and Energy



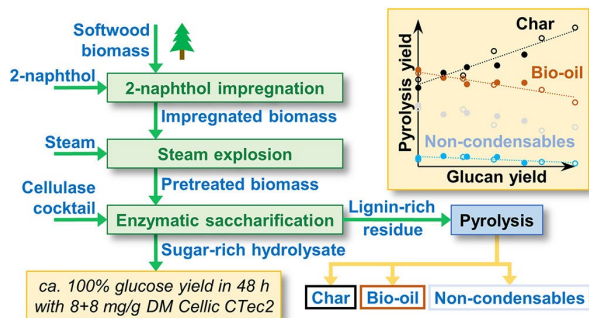
Modelling of an integrated biorefinery for spruce valorization and preliminary Techno-economic assessment (TEA)

Matteo Gilardi, Filippo Bisotti, Olaf T. Berglihn, Bernd Wittgens

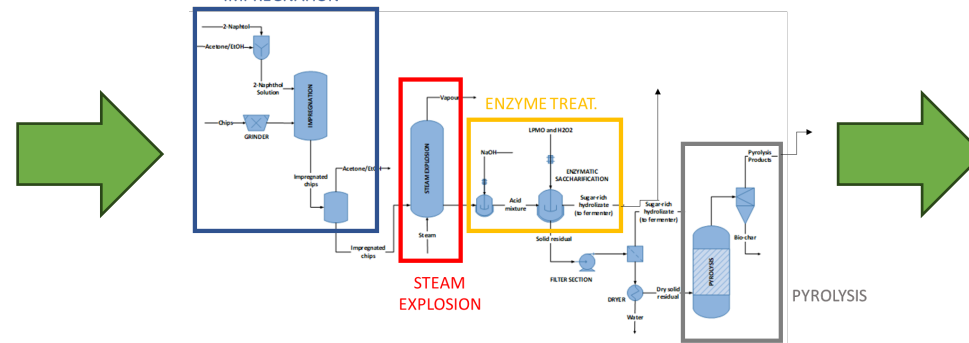
From lab-scale to industrial facility

We target process **design and scale-up** of a **biorefinery for the valorization of spruce chips**:

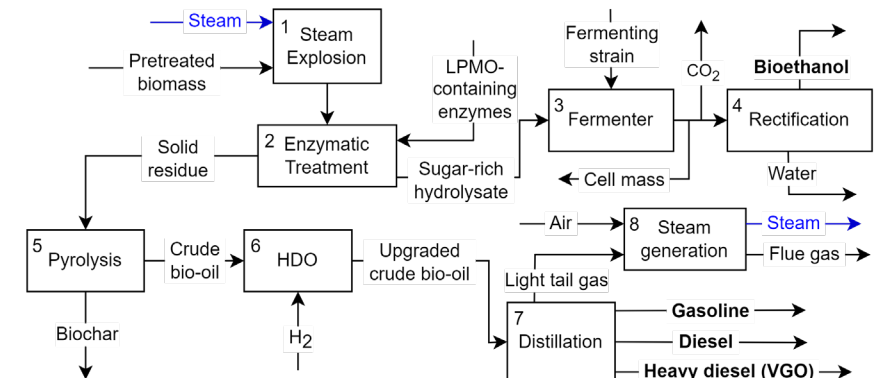
- Remove lab-scale steps that cannot be replicated on an industrial scale
- Identify missing steps and **design a comprehensive process**
- Identify a feasible and **valuable path to convert biomass into added-value chemicals**



1. Tested lab-scale concept

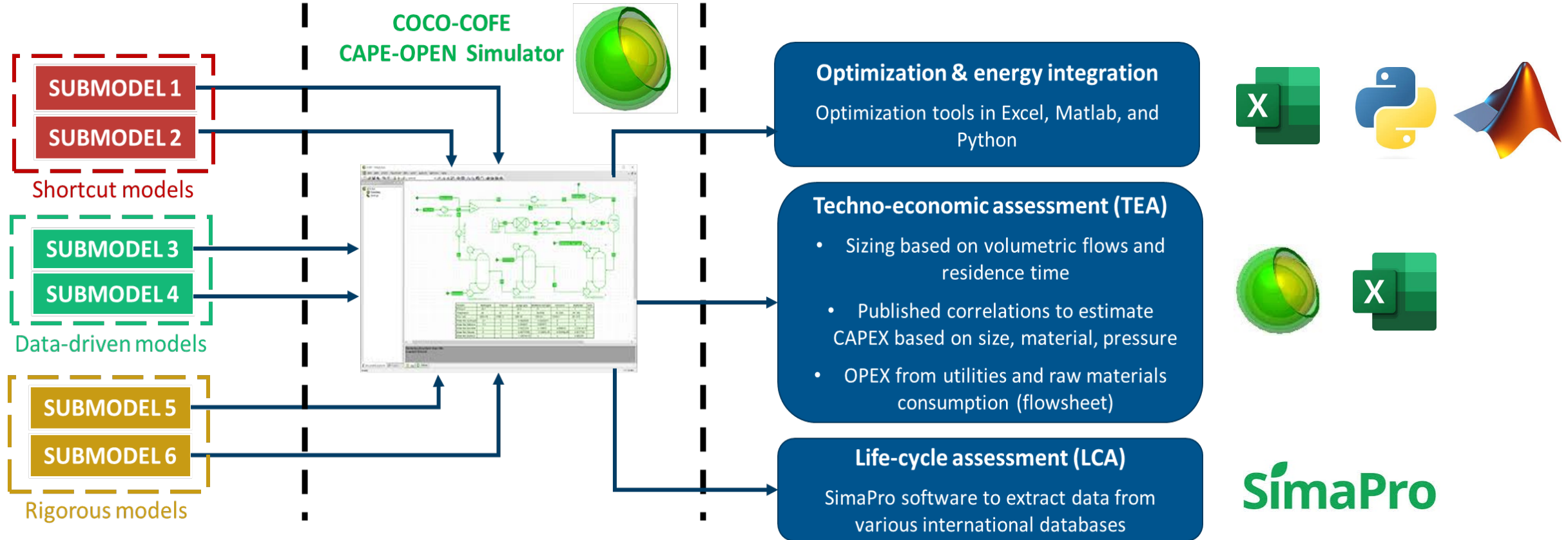


2. Translation into a feasible industrial plant



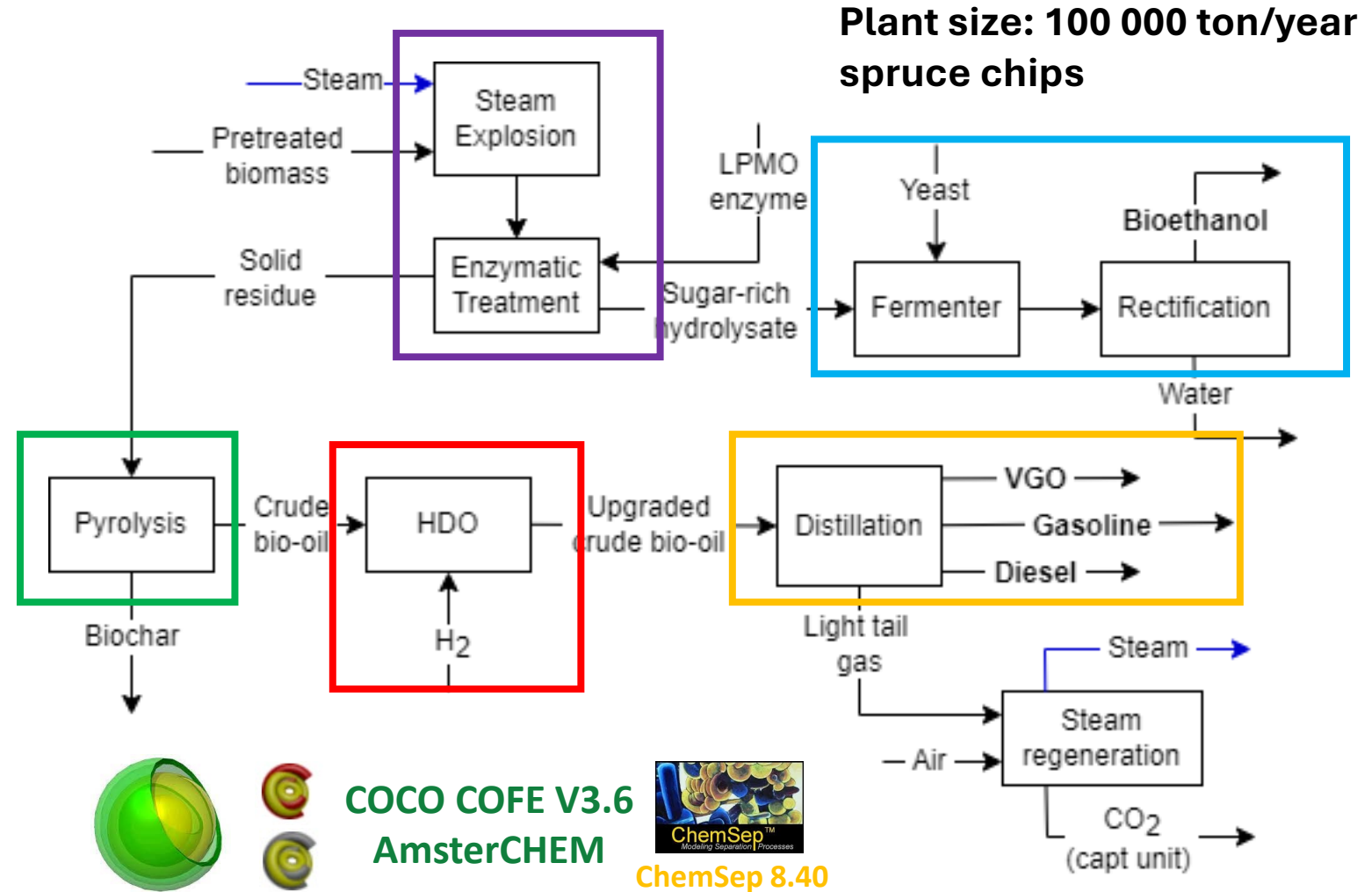
3. BFD completed with missing steps/units

Approach: from plug-in models to TEA



Block Flow Diagram and Simulation tools

- **Spruce chips** are converted into **bio-oil** and **bioethanol** in an integrated biorefinery.
- Cellulose and hemicellulose chains are broken by **enzymatic treatment**. Sugars are fermented to **bio-ethanol**, which is purified by **rectification**.
- **Lignin** is converted into **bio-oil** through **pyrolysis**. Oil is **stabilized by hydrodeoxygenation** and **distilled in different cuts**.

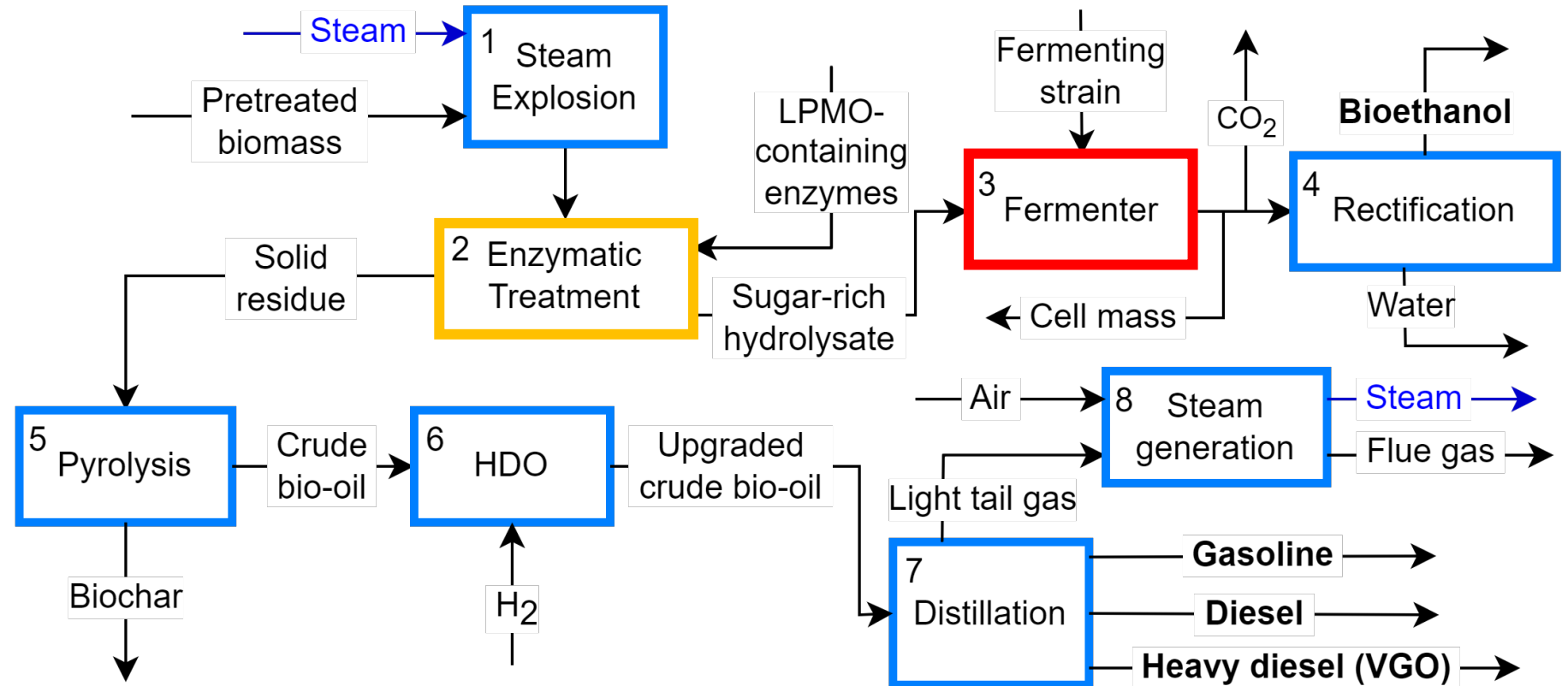


Model implementation

**RIGOROUS
MODELS**

**DATA-
DRIVEN
MODELS**

**BLACK-BOX
MODEL**



Simulation results: KPIs productivity

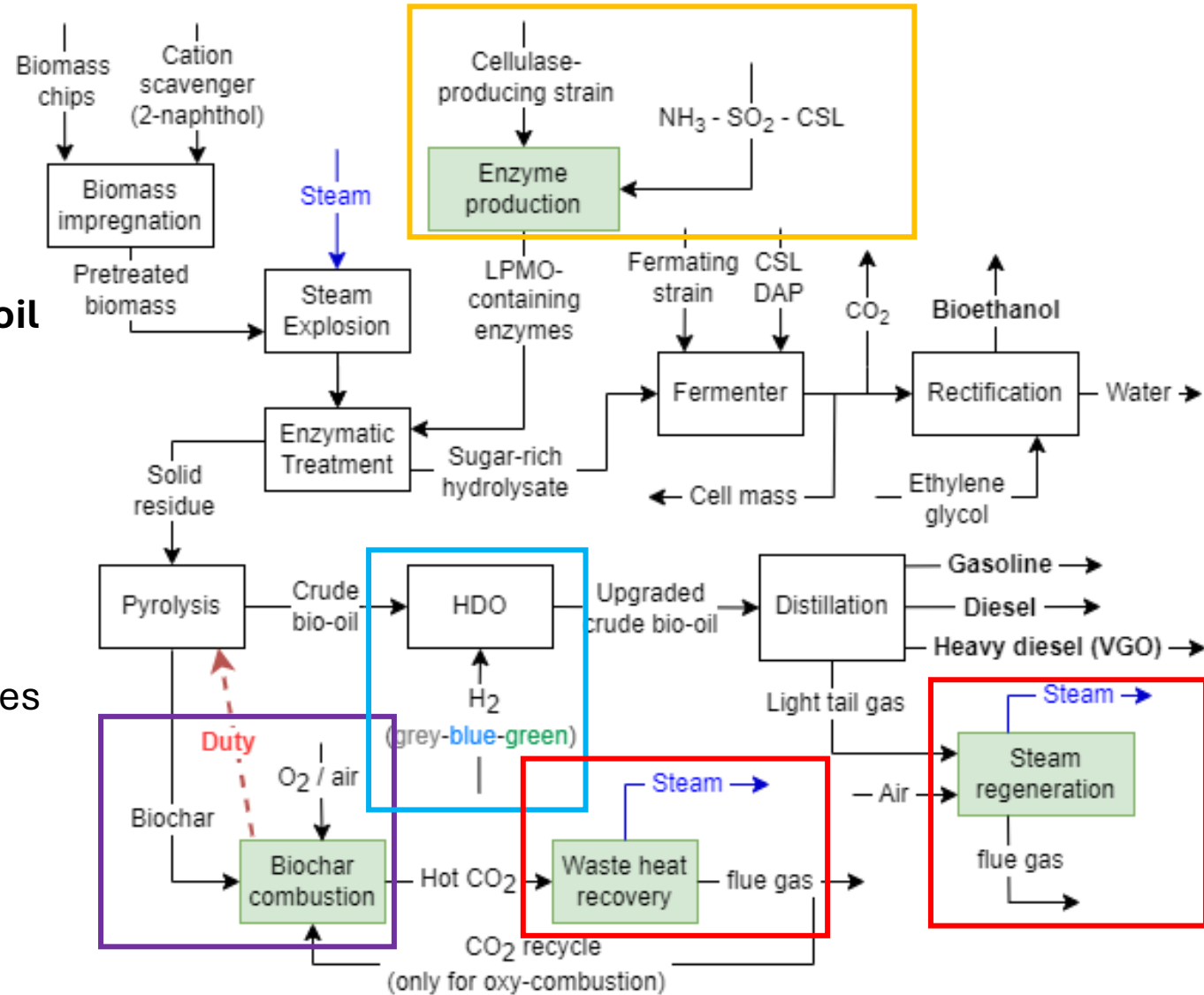
KPIs (Key Performance Indicators)		Notes
Process weight yield (including biochar)	0.593 kg _{product} /kg _{BM}	Light gas is excluded. The mass yield refers to the treated biomass
Process weight yield (excluding biochar)	0.457 kg _{product} /kg _{BM}	Light gas is excluded
Bioethanol yield	0.21 ton _{ethanol} /ton _{BM}	Water/moisture is not included in the mass used to calculate these yields
Bio-oil yield	0.24 ton _{bio-oil} /ton _{BM}	
Biochar yield	0.14 ton _{biochar} /ton _{BM}	
Light gas yield	0.11 ton _{tail gas} /ton _{BM}	

Simulation results: KPIs energy

KPIs (Key Performance Indicators)		Notes
Total specific steam demand	2.43 ton _{steam} /ton _{BM}	
Cooling water demand	32.4 ton _{CW} /ton _{BM}	
Pyrolysis specific energy	1.65 MJ/kg _{dry BM} 0.46 MWh _{th} /ton _{BM}	In line with Daugaard and Brown (2003)
Total specific thermal duty	0.98 MWh _{th} /ton _{BM}	Includes all the thermal duties (supplied heat)
Specific cooling duty	0.56 MWh _{th} /ton _{BM}	Includes all cooling duties (removed heat)
Specific electricity	1.45 MWh _{el} /ton _{BM}	Simulations assume 70% efficiency for pumps and compressors. Spare pumps are neglected.

8 Integration & Optimization

- ❑ On-site enzyme production
- ❑ Heat recovery from hot stabilized oil
- ❑ Different H₂ sources
 - ✓ Green H₂ production can cover also the O₂ demand for char oxy-fuel combustion
- ❑ Steam generation from hot flue gases
- ❑ Biochar combustion in air/O₂ to provide the thermal energy for the pyrolysis chamber



Unit sizing and investment cost

The **sizing of upscaled reactors from batch lab scale data** is obtained based on the **residence time** and **circulating volume flow (Q)**.

$$Vol = Q \cdot \tau_{res}$$



The total investment cost is obtained by summing the **base equipment costs**, the **installation costs**, and **indirect investment costs** using **correction factors (f)**.



$$C_{tot} = C_{equipment} + C_{install} + C_{indirect}$$

The **base equipment cost** is calculated as a **function of the unit size** using correlations by Guthrie, Ulrich, and Navarrete^[1-3].

Costs are **actualized to 2023 with CEPCI** index.

$$C_{install} = C_{equipment} \cdot (f_{installation} + f_{piping} + f_{instrumentation} + f_{auxiliary} + f_{electrical} + f_{building} + f_{yard\ improv} + f_{infrastructure})$$

$$C_{indirect} = C_{equipment} \cdot (f_{engin\ \&\ superv} + f_{construction} + f_{legal\ fees} + f_{contractor\ fees} + f_{contingency})$$

[1]. Guthrie, 1974. Process Plant Estimating, Evaluation and Control

[2] Ulrich, G. D., 1984. A Guide to Chemical Engineering Process Design and Economics. John Wiley and Sons.

[3] Navarrete, P. F., 1995. Planning, Estimating, and Control of Chemical Construction Projects. Marcel Dekker, Inc.

Operating costs

Operating costs are estimated according to Turton^[1].

Direct manufacturing costs	
Raw materials	Cost of amine make-up + water make-up
Utilities	Cost of natural gas + electricity + cooling water
Operating labour (C_{OL})	Annual operator salary* total number of operators required by the site
Direct Supervisory and clerical labour	$0.18 \cdot C_{OL}$
Maintenance and repair	$0.07 \cdot FCI$
Operating supplies	$0.009 \cdot FCI$
Laboratory charges	$0.15 \cdot C_{OL}$
Fixed manufacturing costs	
Depreciation	$0.1 \cdot FCI$
Local taxes and insurance	$0.03 \cdot FCI + 0.01 \cdot FCI$
Plant overhead costs	$0.708 \cdot C_{OL} + 0.036 \cdot FCI$
General expenses	
Administrative costs	$0.177 \cdot C_{OL} + 0.009 \cdot FCI$

Raw material	Specific cost (\$/ton)	Source
Spruce chips	56.7	[4]
2-Naphtol	3500	[5]
Hydrogen blue green grey	3500 7250 1500	[6]
NH ₃	410	[5]
SO ₂	276	[5]
Corn steep liquor (CSL)	50	[5]
DAP	895	[5]
Ethylene glycol	860	[5]
Oxygen from ASU	250	[6]

Average over last 10 years
(data by Statistisk
sentralbyrå)

Utility	Specific cost	Source
Natural gas	20 \$/MWh	[2]
Electricity	61.3 \$/MWh	[3]
Cooling water	0.354 \$/GJ	[1]

FME Bio4Fuels - Norwegian Centre for Sustainable Bio-Based Fuel and Energy

[1] Turton, R. Analysis, Synthesis and Design of Chemical Processes. 5th Edition, Prentice Hall
 [2] <https://tradingeconomics.com/commodity/eu-natural-gas>;
 [3] SSB Electricity prices. <https://www.ssb.no/en/energi-og-industri/energi/statistikk/elektrisitetspriser>

[4] NMBU. https://publikasjoner.nve.no/rapport/2012/rapport2012_32.pdf.
 [5] D. Bbosa, M. Mba-Wright, R.C. Brown, 2018, Biofuels, Bioproducts & Biorefining, 12, 497-509
 [6] J.M.M Arcos and D.M.F. Santos, 2023, Gases, 3, 25-46.

Sensitivity analysis on H₂ source

Sensitivity analysis on hydrogen source (for HDO) and air/oxyfuel combustion has been performed.

Case	H ₂ source	Combustion type
CS1	Grey	Air
CS2	Grey	Oxy-fuel (O ₂ from Air Separation Unit)
CS3	Blue	Air
CS4	Blue	Oxy-fuel (O ₂ from Air Separation Unit)
CS5	Green	Oxy-fuel (integrated H ₂ and O ₂ production via electrolysis)

Assumption for oxy-fuel combustion: the **boiler volume is reduced by ¾** due to the absence of nitrogen.

Cash flow

- We investigate the **MSPR (Minimum Selling Price Ratio)** for bio-oil and bio-ethanol to target an **Internal Rate of Return (IRR)** equal to **10% or 15%**.
- MSPR is obtained using the actual selling prices of the corresponding **fossil-based product** as a **reference**.

MSP (same): same price ratio assumed for both bio-oil and bio-ethanol

MSP (oil) and MSP (ethanol): price ratio calculated only for the commodity in brackets. The price for the other product is fixed to the current value.

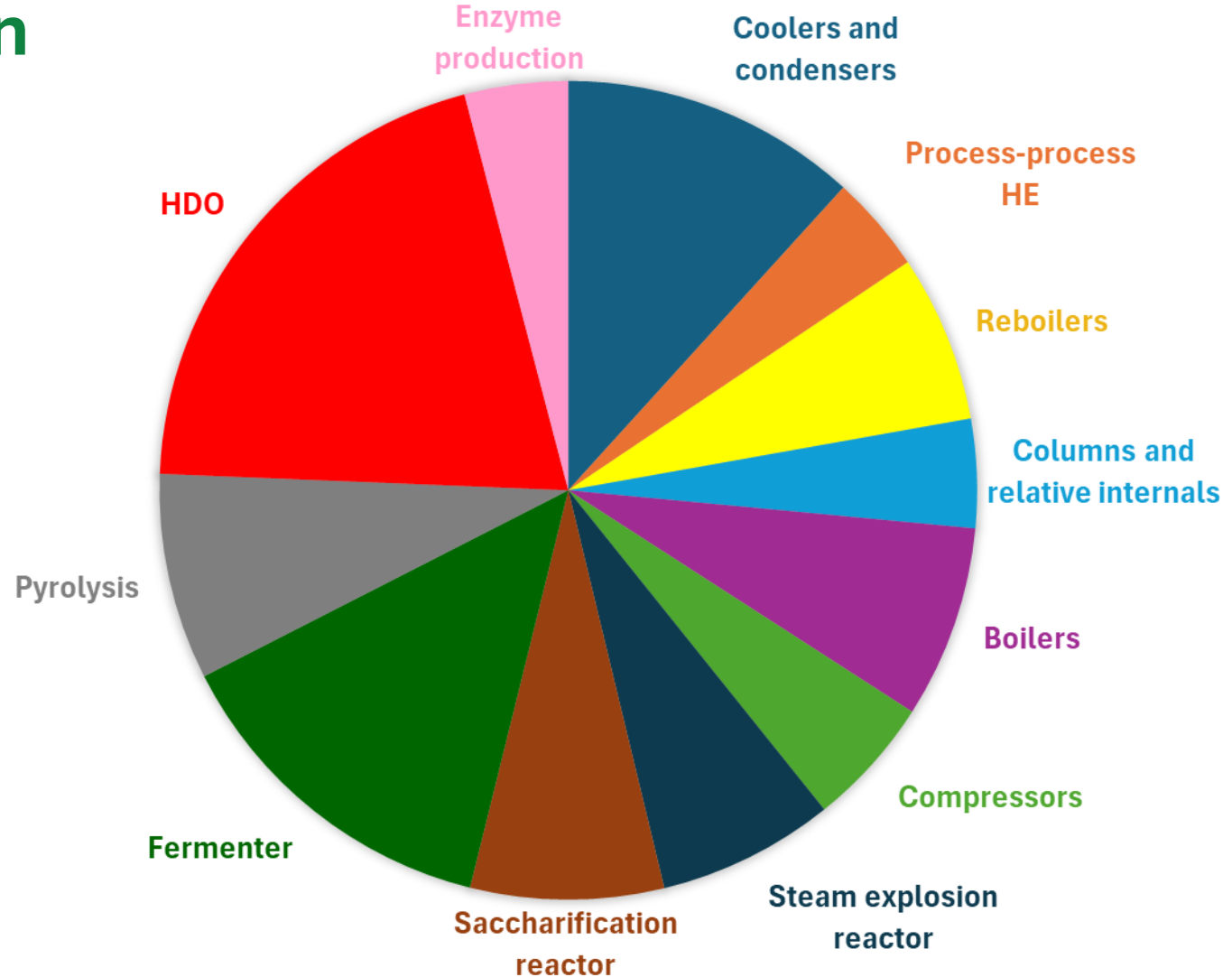
Three options for hydrogen: **grey**, **blue**, and **green**.



Fossil-based Product	Selling price (\$/liter)	Source
Ethanol	0.80	[1]
Gasoline	0.79	
Diesel	0.86	

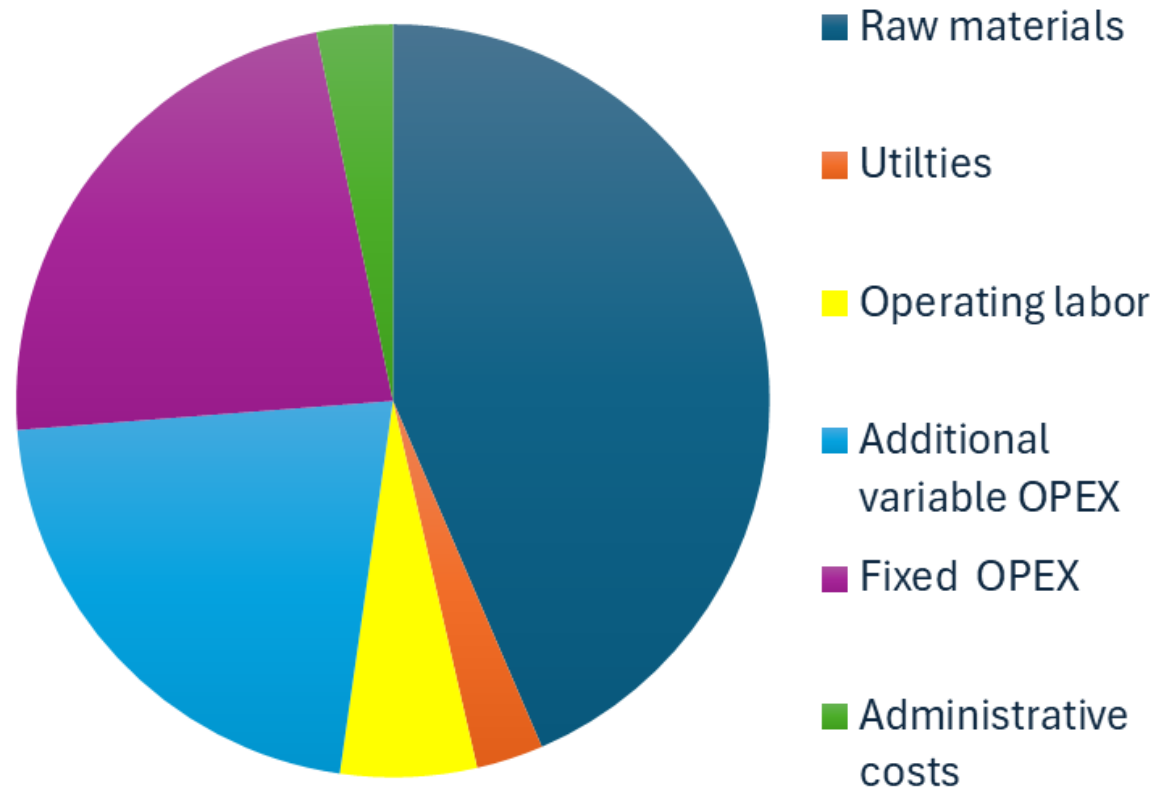
CAPEX breakdown

- Saccharification, fermentation, and pyrolysis are associated with **high large CAPEX** due to the **high required residence time**.
- **HDO** is a major contribution being a **high-pressure catalytic chamber**.



OPEX breakdown

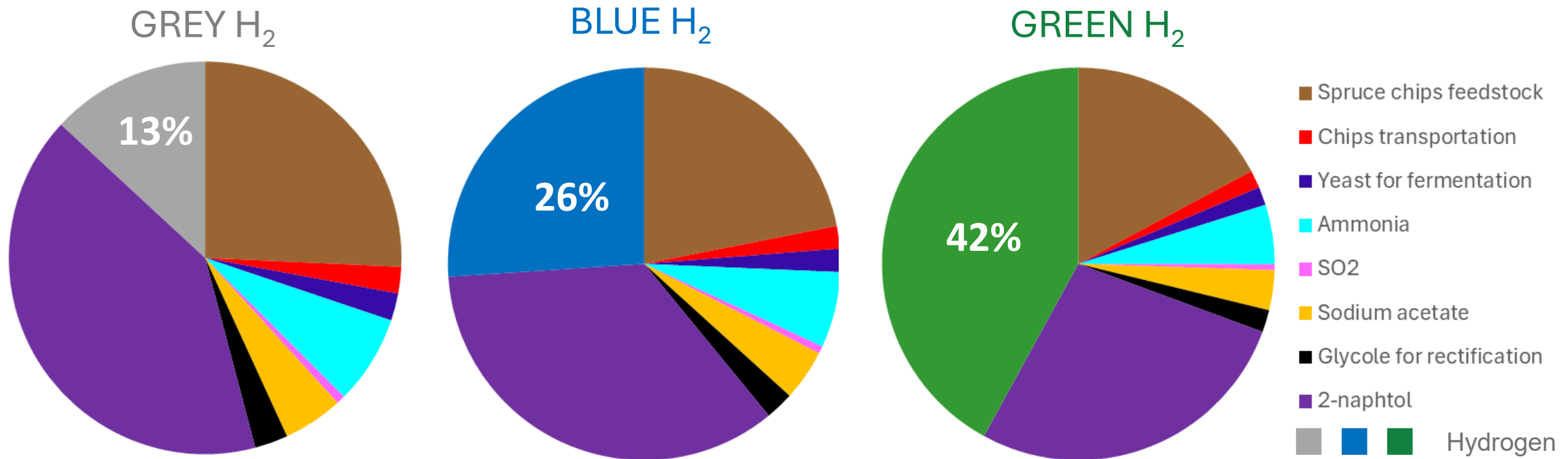
Reference case-study: green H₂ and air combustion



Raw materials are the **key contribution** to the operating costs.

Thanks to the proposed energy integrations, the **demand for external utilities is minimized.**

OPEX breakdown: raw materials



- The share of raw materials cost associated with H₂ significantly increases when blue or green H₂ are used.
- **2-naphtol can be potentially replaced with phenolics** to be recovered from the produced bio-oil.

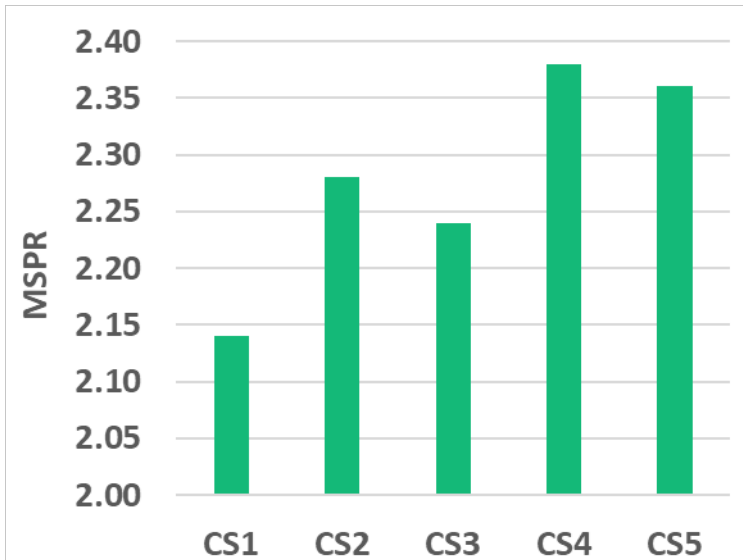
Results: CAPEX and OPEX

Case study	Hydrogen color	Combustion	CAPEX [M\$]	Raw materials [M\$/year]	Utilities [M\$/year]	Total OPEX [M\$/year]
CS1	Grey	Air	179	22.04	1.96	76.48
CS2		Oxy-fuel	169	29.73	1.96	83.99
CS3	Blue	Air	179	25.89	1.96	81.22
CS4		Oxy-fuel	169	33.58	1.96	88.73
CS5	Green	Oxy-fuel	179	33.02	1.96	88.04

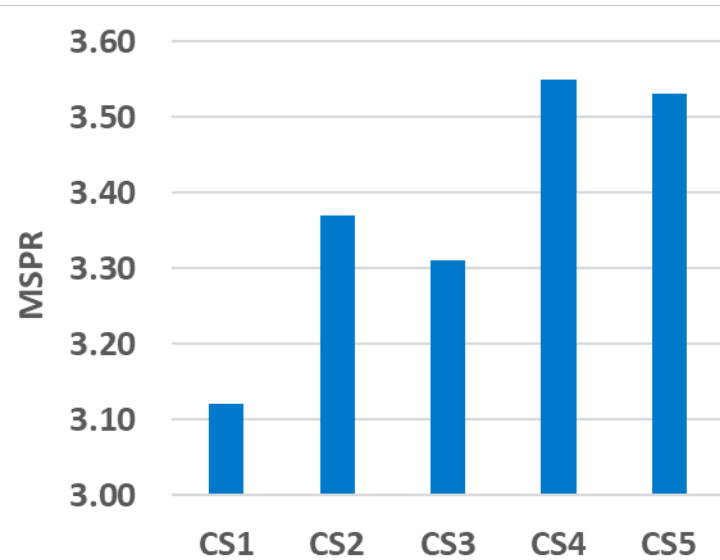
- **Oxy-fuel combustion** provides a **5% reduction in the total CAPEX** due to the lower boiler volume.
- **Oxygen for ASU** results in a **10% increase in the total OPEX** compared to air combustion.
- **Green hydrogen** results in a **15% increase in the total OPEX** with respect to grey hydrogen and air combustion.
- CS5 provides slightly better results than CS4.

Results: MSPR

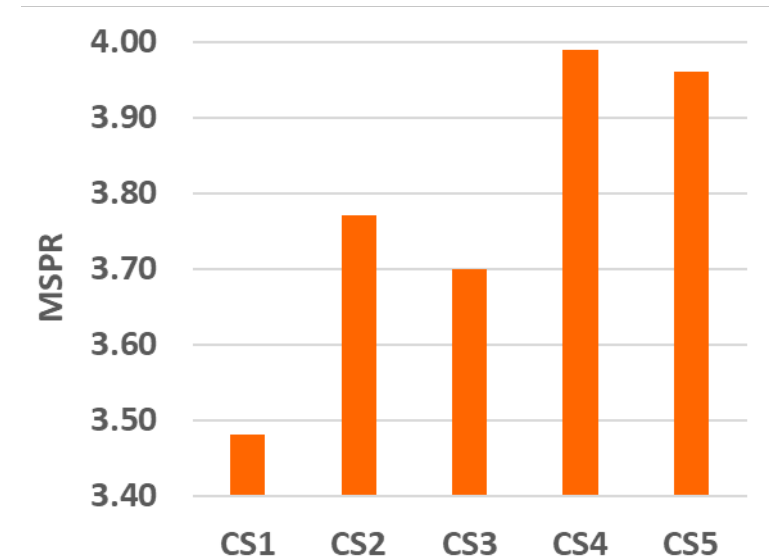
Target: IRR= 10%



MSPR (same)



MSPR (ethanol)



MSPR (oil)

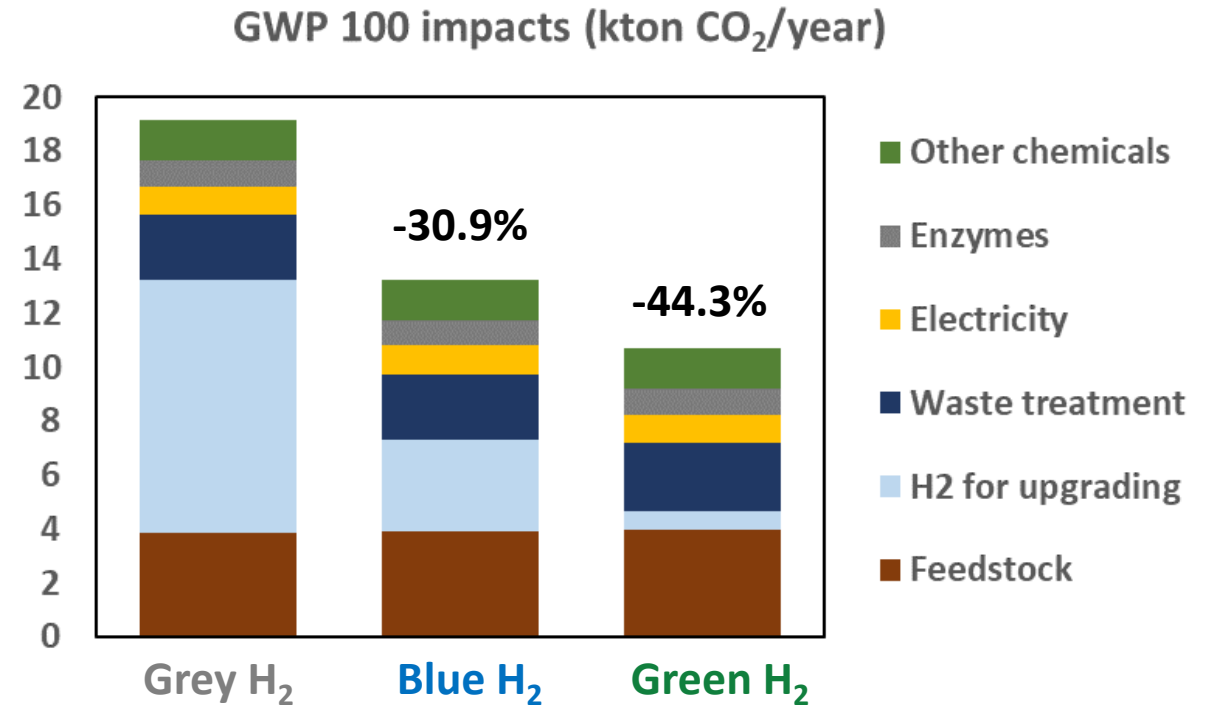
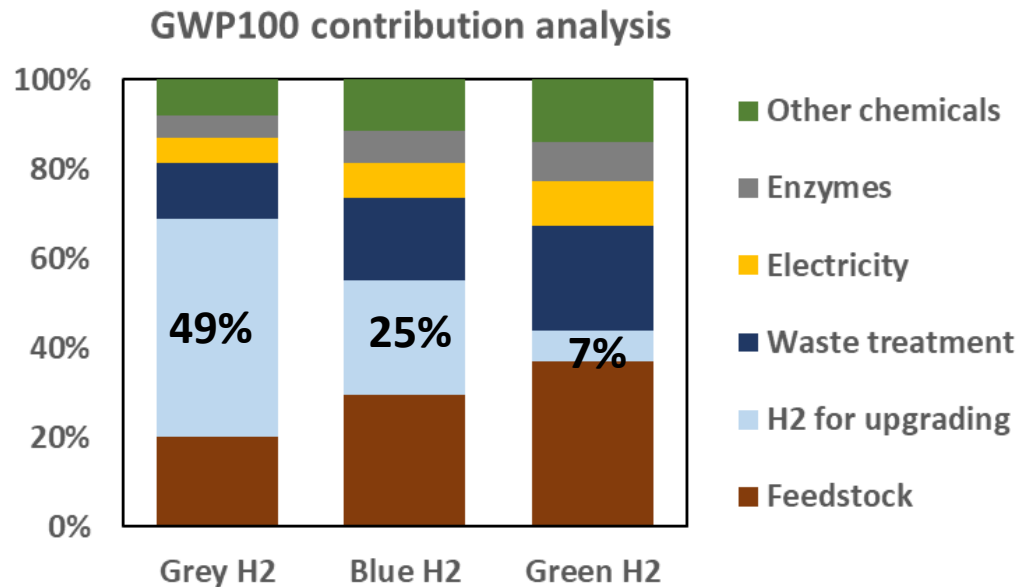
- All scenarios require a **MSP** for both **bio-ethanol** and **bio-oil** over two times the actual prices of the **corresponding fossil-derived products**.
- Using green hydrogen requires a 9% and 4.5% higher MSPR with respect to grey and blue hydrogen, respectively.
- **Green hydrogen** is currently much **less economically viable**, but **what about the effect on CO₂ eq. emissions?**

Environmental assessment

An environmental analysis (GWP100 impact category only) of the process was performed in cooperation with Prof. Cherubini and Dr. Ballal.

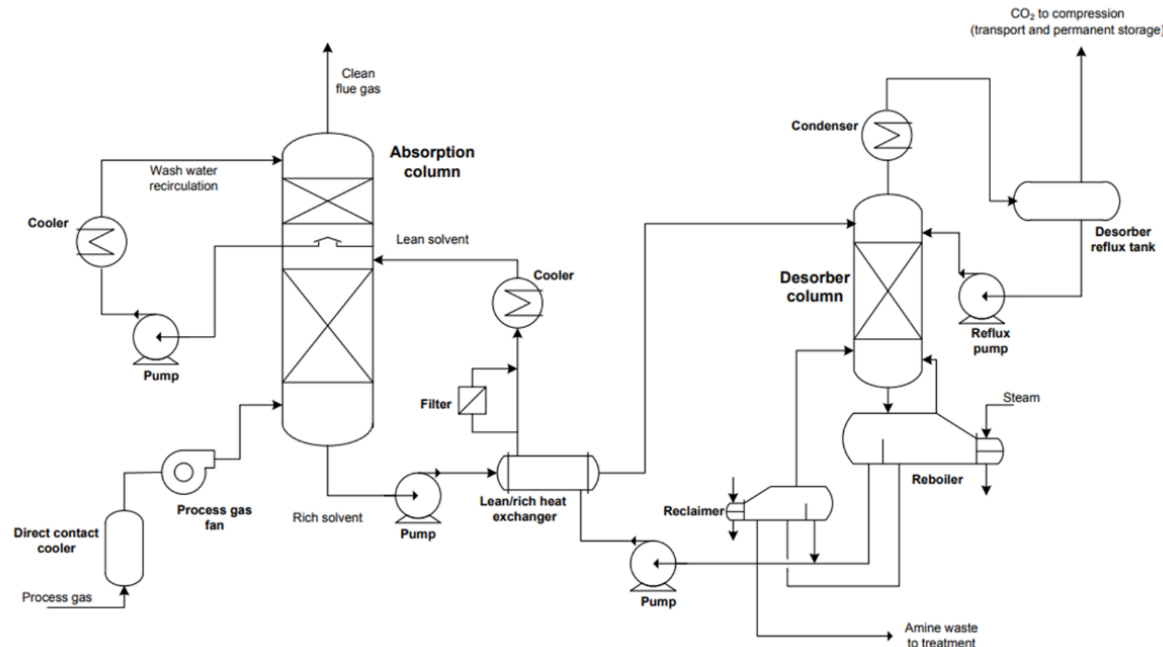
KEY ASSUMPTIONS

- System boundaries set to the process itself (gate-to-gate)
- Electricity source: Norwegian National electricity mix
- Grey hydrogen: SMR of natural gas
- Green hydrogen: offshore wind energy for electricity production



CO₂ capture: towards negative CO₂ emissions

- **CO₂-rich streams** from light gas combustion (6 vol%) and char combustion (14.5 vol%) have potential for CO₂ capture.
- The two stacks have been mixed and **conveyed to a conventional amine absorption plant.**
- Two solvents have been considered: **MEA** and **CESAR-1**



Simulation software: **CO2SIM**

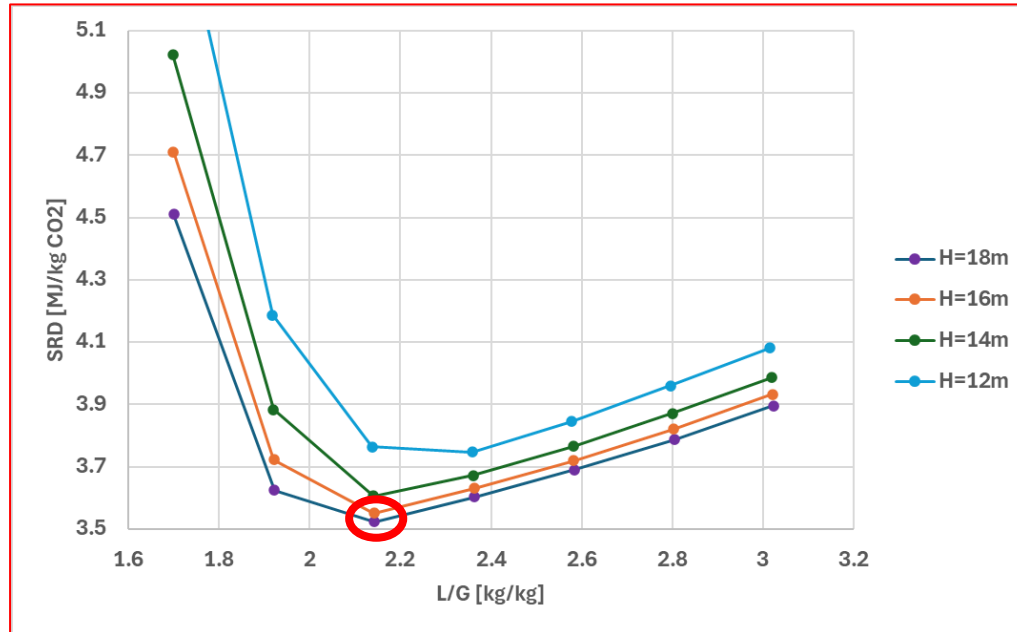


ASSUMPTIONS

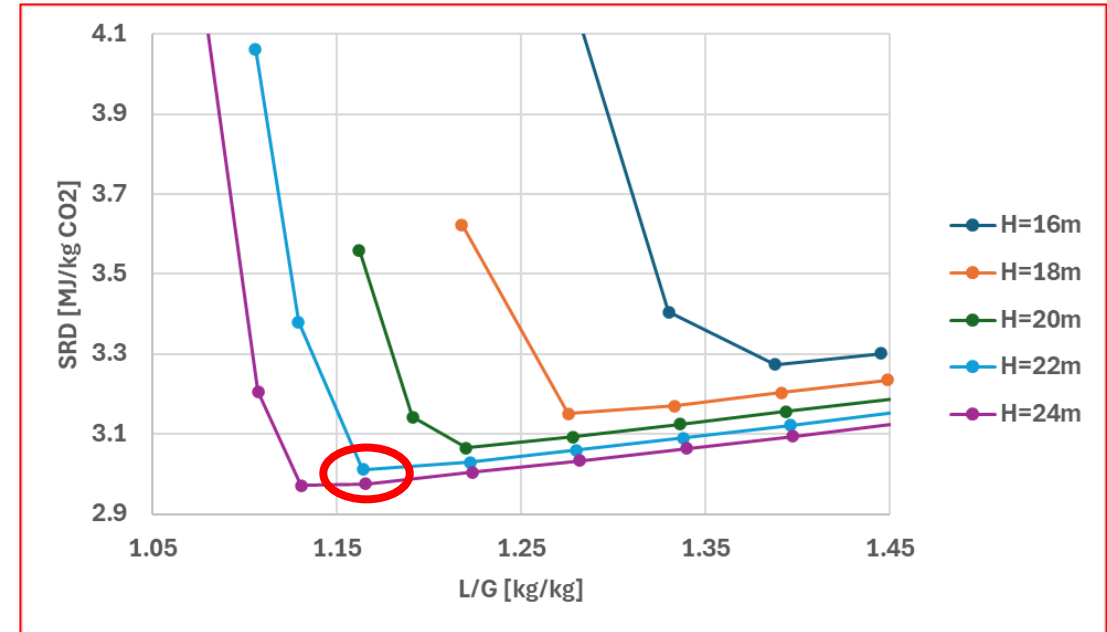
- 90% CO₂ capture
- Packing: Mellapak 2X
- Sensitivity analysis to determine optimal L/G ratio and absorber packing height to minimize the Specific Reboiler Duty (SRD)

CO₂ capture plant optimization

MEA



CESAR-1

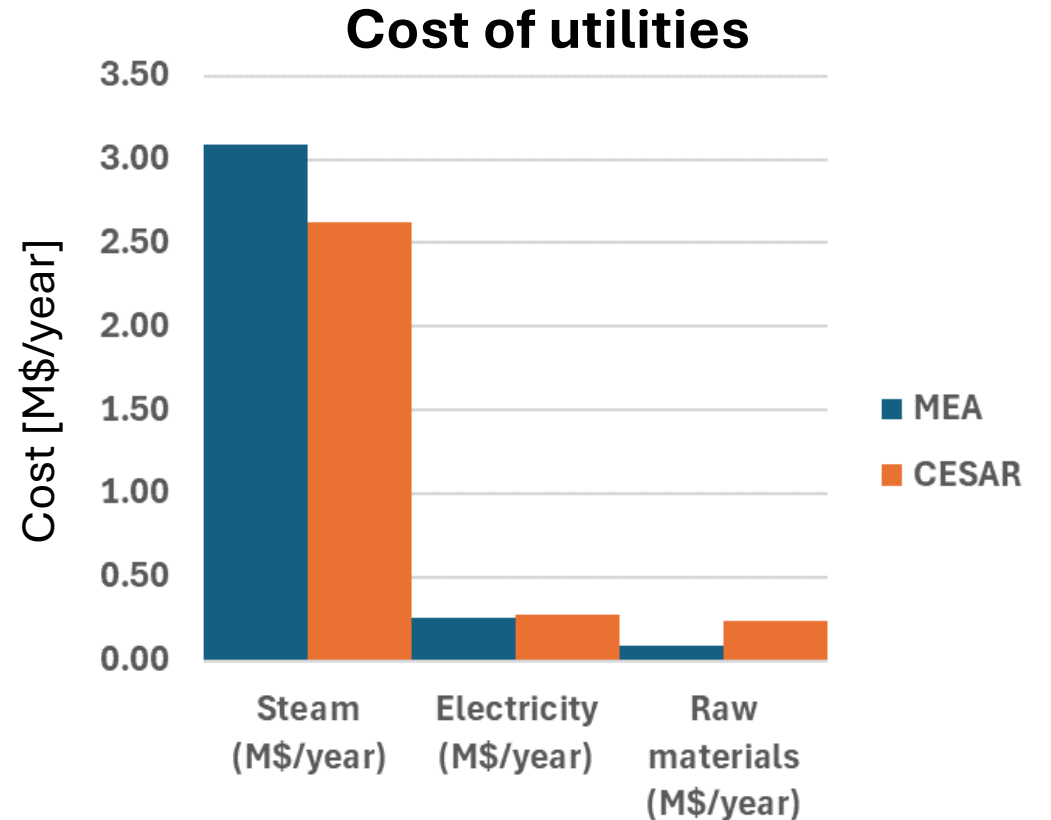


Using CESAR-1:

- the **SRD of the optimized capture plant** reduces from 3.55 down to **3.01 MJ/kg CO₂ capt. (-15%)**
- The required **solvent flow** is also **reduced by a factor of 45%**
- Conversely, a **higher packing is needed** due to slower kinetics (22m versus 16m)

CO₂ capture plant costs

Index	MEA	CESAR	CESAR vs MEA
FCI (M\$)	23.05	22.69	-1.5%
Total OPEX (M\$/year)	12.61	12.16	-3.5%
Utilities (M\$/year)	3.43	2.97	-13.2%
Steam (M\$/year)	3.09	2.62	-15.2%
Electricity (M\$/year)	0.25	0.28	+10.0%
Raw materials (M\$/year)	0.09	0.24	2.61 times
Total cost (M\$/year)	12.61	12.16	-3.5%



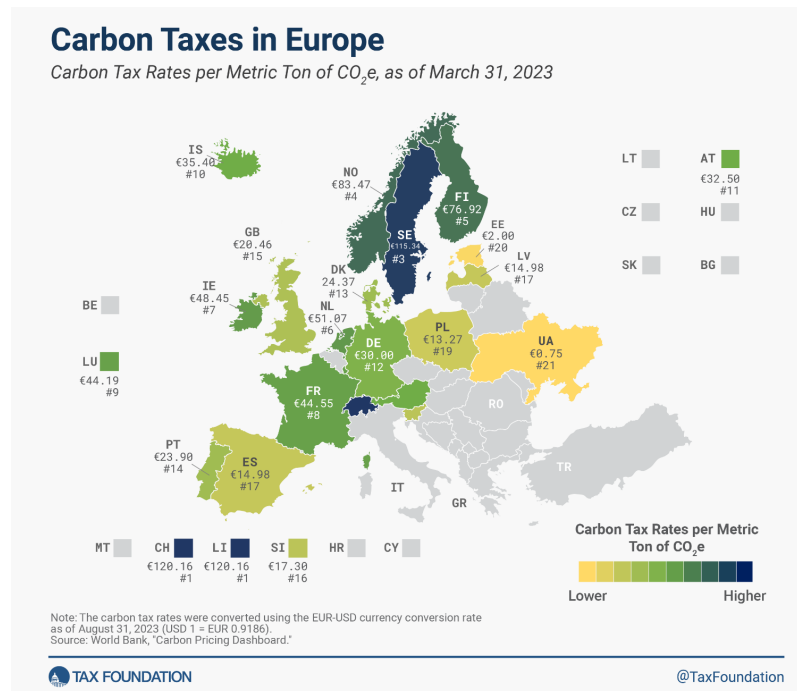
Is the cost of CO₂ capture sustainable for the designed biorefinery?

- **Biorefinery CAPEX increase** when integrating the capture plant: + **12.7%**
- **Biorefinery OPEX increase** when integrating the capture plant: + **15.9%**



Breakeven carbon tax: 240 \$/ton CO₂

- The high specific CO₂ capture cost in this application is due to the limited volume of treated flue gas (economy of scale)
- Integrated capture plant with flue gases from other facilities at close distance is a great option to enhance viability (**industrial symbiosis**)



Conclusions

- **Successful scale-up modelling** of an integrated biorefinery for combined bioethanol and bio-oil production from spruce chips.
- The proposed **integrated biorefinery minimizes biomass waste** through the complete **valorization of all biomass constituents**, including lignin, and promoting **energy recovery**.
- If grey hydrogen is exploited, the **Minimum Selling Price** required for **ethanol and bio-oil** to achieve a IRR=10% is **2.14 times the actual price for fossil-derived sources**.
- Cooperation with SP1 to **combine economic and environmental considerations**.
- Good potential for **CO₂ capture integration** toward **negative CO₂ emissions**.
- Need to discuss the potential for **industrial symbiosis**: how to **effectively link this biorefinery with other plants?**

Conferences and publications



Palermo, Italy
19-22 May, 2024

Strategies and approaches for the modelling of a biorefinery

ESCAPE 34 - PSE 24



2-6 June 2024

Florence, Italy



Matteo Gilardi, Filippo Bisotti, Olaf T. Berglihn, Roman Tschentscher, Line D. Hansen, Svein J. Horn, Anikó Várnai, Bernd Wittgens

From laboratory scale to innovative spruce-based biorefinery. Note I: Conceptual process design and simulation

From laboratory scale to innovative spruce-based biorefinery. Note II: Preliminary techno-economic assessment

Upcoming presentations



Economic and environmental assessment



CO₂ capture integration



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